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ELECTRICALLY DRIVEN CAMSHAFT ADJUSTER

5 Description

FIELD OF THE INVENTION

10 The invention relates to a camshaft adjuster for adjusting and fixing the position of the angle of rotation of the camshaft relative to the crankshaft of a reciprocating-piston internal-combustion engine, especially according to the preamble of Claim 1.

BACKGROUND OF THE INVENTION

15 In DE 41 10 195 A1, a camshaft adjuster for adjusting and fixing the relative position of the angle of rotation of a camshaft relative to the crankshaft of a reciprocating-piston internal-combustion engine is disclosed, with a high transmission and friction-reduced adjusting gear mechanism comprising a drive shaft, which is connected rigidly to the crankshaft, a driven shaft, which is rotationally fixed to the camshaft, and an adjusting shaft, which is connected to an adjusting motor shaft of an adjusting motor.

25 In this solution, the adjusting motor shaft is formed integrally with the adjusting shaft of the adjusting gear mechanism. Therefore, when the adjusting motor fails, the entire camshaft adjuster always has to be replaced. In addition, the assembly itself is complicated, because pre-assembly of the complete adjusting motor is impossible.

OBJECT OF THE INVENTION

The invention is based on the objective of creating a camshaft adjuster, which is economical to run.

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SUMMARY OF THE INVENTION

According to the invention, the problem is solved by the features of the independent Claim 1. Through the separate formation of adjusting motor and
10 adjusting gear mechanism, the adjusting motor can be completely pre-assembled and installed or replaced in a simple way due to the disengaging coupling. Because the coupling is free from rotational backlash, its operation is guaranteed to exhibit low wear and low noise.

15 The arrangement according to the invention of a disengaging coupling between the adjusting gear mechanism and adjusting motor is independent of the type of adjusting motor. Especially preferred is the electric adjusting motor. In contrast with a hydraulic motor, the electric motor has the advantage of functioning independent of the engine speed of the internal-
20 combustion engine and thus it also functions when the internal-combustion engine is stopped. In addition, the oil viscosity has no effect on its function. In contrast with a pneumatic motor, the electric adjusting motor has the advantage, in the normal case, of an already existing power supply and uncomplicated control.

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Manufacturing and thus cost advantages are provided when the coupling has two parts that can be joined together, of which one is rotationally fixed to the

adjusting motor shaft and the other is rotationally fixed to the adjusting shaft.

5 A simple assembly of the adjusting motor is achieved in that one of the two parts is formed as an outer part and the other is formed as an inner part, wherein the two parts can be inserted one into the other in a play-free way.

10 An advantageous improvement of the invention is provided in that the coupling is formed as a profiled shaft coupling, preferably as a two-side shaft coupling, which has two coupling surfaces on each outer part and two coupling surfaces on each inner part, wherein preferably the latter has rotational backlash-reducing means. The proven two-side shaft coupling offers sufficient room for mounting torque-transferring and rotational backlash-reducing means. As couplings, feather key and profiled shaft
15 couplings, such as polygonal, toothed, wedge, and multi-edge shaft couplings, are also possible. Also, a shaft milled on one side with a corresponding counter piece (similar to the two-side shaft but with only one straight surface) is likewise conceivable. The mounting of the rotational backlash-reducing means on the inner part offers assembly and structural space
20 advantages in comparison with mounting these means on the outer part, which is also possible.

A conventional solution can be seen in that as rotational backlash-reducing means, a minimal, tightly toleranced play is provided between the coupling
25 surfaces of the inner and outer parts. The resulting necessary manufacturing precision requires corresponding construction expense.

A more economical solution is provided in that as rotational backlash-reducing means, biased metal or plastic springs are provided, which bridge the play between the coupling surfaces. Due to the biasing of the springs and their sufficient spring path, the play between the coupling surfaces and its tolerance can be selected relatively large, whereby the construction expense is reduced accordingly.

It is advantageous that the metal springs are formed as flat bending or plate springs and the plastic springs are formed preferably as polymer bands or polymer O-rings and arranged preferably in grooves or in a circular groove of the coupling surfaces of the inner part. The mounting of the polymer springs in annular grooves of the coupling surfaces of the inner part simplifies above all the assembly of the polymer band and the polymer O-ring, which are arranged there so that they are secure from becoming lost.

The spring and assembly forces required for torque transfer and rotational backlash reduction are relatively low, because the torque to be transferred, less than 1 Nm, is relatively minimal, so that no relative rotation of the electric motor and the adjusting shaft occurs for the corresponding spring stiffness. The springs can also compensate for small alignment errors of these shafts. There are advantages when the flat bending or plate springs are formed as one-piece spring clasps, which preferably clip onto corners of the inner part. In this way, pairs of the flat bending or plate springs form one unit, which is fixed on the inner part so that it is secure from becoming lost and thus simplifies the assembly of the adjusting motor.

One advantageous configuration of the invention is provided in that the coupling is formed as a tubular shaft coupling, with a hollow cylindrical outer part and a coaxial, cylindrical inner part, which is arranged with play in the outer part and which preferably has rotational backlash-reducing means. The two parts are formed as turned parts, which are simple and economical to produce. Likewise, it is advantageous if as rotational backlash-reducing means an elastically deformable, preferably metal tolerance ring is provided, which is arranged in a radial groove, preferably on the periphery of the coaxial, cylindrical inner part, and which extends past this part by a certain extent in the radial direction. In principle, the tolerance ring could also be arranged on the inner periphery of the outer part, but the arrangement according to the invention is more assembly-friendly.

Due to the projection of the tolerance sleeve, in the assembly, a spring-elastic deformation of the same is produced, which leads to a frictional connection between the inner and outer parts. In the selection of the projection, it must be taken into account that the torque of the adjusting motor can be transferred without essentially preventing the axial movement of the inner and outer parts relative to each other and thus expansion due to heat. The tolerance ring is also conceivable as a polymer ring.

Through one advantageous configuration of the invention, it is achieved that at least one locking ball or one preferably cylindrical locking pin with a conical end is provided as rotational backlash-reducing means, which are guided in radial bore holes or through holes, preferably of the coaxial, cylindrical inner part with play and which can be displaced into other radial bore holes of smaller diameter, aligned with the bore holes mentioned above,

in the hollow cylindrical outer part under the force of a compression or through spring by a measure limited by the smaller diameter. Instead of the one locking element, advantageously there can also be two or more locking balls or cylindrical locking pins. These could also be arranged in the outer
5 part and engage radially in a corresponding bore hole of the inner part. As an alternative to the cylindrical pins, pins, for example, with square or rectangular or also any other cross section can also be used. In this variant, small alignment errors between the adjusting motor shaft and adjusting shaft can also be compensated. The through hole has the advantage of simpler
10 production and a uniform application of pressure on the locking balls or locking pins in comparison with the two radial bore holes, which are replaced by this through hole.

Through corresponding design of the spring force of the compression or
15 through springs and/or the cone angle of the cylindrical pins, the transferable torque of the tubular coupling can be limited. This then acts as a safety coupling, in that for an overload, the locking balls or the cylindrical locking pins are displaced from the bore holes in the outer part against the relatively small spring forces and thus the two shafts are disengaged. For axial
20 movement of the tubular shaft coupling equipped with locking balls or with cylindrical locking pins, it is necessary that the other radial bore holes are formed as elongated holes aligned in the axial direction.

It is advantageous when the coupling is formed as a clutch coupling, whose
25 two parts have axial claws, which are arranged at the same diameter and which engage in each other, wherein between the claws, there are distances, which are bridged by tooth elements of an elastic, biased polymer collar in a

rotational backlash-free way. The clutch coupling also enables the equalization of a small axis offset due to the elasticity of the polymer collar. In addition, it acts as a vibration damper.

- 5 Another advantageous coupling is formed as a profiled shaft coupling, preferably a toothed shaft coupling, whose inner and outer part, especially whose internal and external gearing, is formed from elastic plastic. In view of the relatively low torque to be transferred, many kinds of couplings, for example, polygonal or multi-edge shaft couplings, are suitable for half-side
10 formation in plastic. The toothed shaft coupling is distinguished by especially simple assembly. Due to the elastic plastic toothed collar, it also enables the compensation of slight axis offset. Likewise, it acts as a vibration damper due to the intrinsic damping of the plastic.
- 15 For economical production and compact construction, it is advantageous that the internal or external gearing composed of plastic is molded directly onto corresponding parts of the toothed shaft coupling or onto a correspondingly formed metallic intermediate bushing and that the intermediate bushing is connected to the toothed shaft coupling, preferably through a force-fit
20 connection.

An advantageous configuration of the invention is provided in that the coupling is formed as a magnetic shaft coupling, whose two parts have opposing permanent magnets, which transfer the driving moment of the
25 adjusting motor through magnetic forces in a contact-less and rotational backlash-free way from the adjusting motor shaft to the adjusting shaft. The permanent magnets can be produced from ferrite or rare-earth material, such

as samarium cobalt or neodymium iron boron. Due to the minimal torque to be transferred from the adjusting motor shaft to the adjusting shaft, this is entrained by the magnetic force approximately synchronously, that is, in a rotational backlash-free way. This coupling can also be formed as a safety
5 coupling, which slips if there is an overload. Because the coupling is a contact-less coupling, the torque is transferred with reduced vibration. In addition, a small axis offset can also be compensated.

It is advantageous when the permanent magnets are arranged preferably in
10 the axial direction and between them there is a non-magnetic membrane with two-sided play, which closes the adjusting motor in an oil-tight way. In an axial arrangement of the magnets, it must be taken into account that their maximum distance permitted for the transfer of the torque is not exceeded. On the other hand, the permanent magnets may not touch the membrane. In
15 contrast, the similarly possible radial arrangement of the magnets is for the most part not sensitive to axial displacement, but the formation of a membrane between these permanent magnets is more difficult.

BRIEF DESCRIPTION OF THE DRAWINGS

20 Additional features of the invention emerge from the following description and the associated drawings, in which embodiments of the invention are shown schematically. Shown are:

- 25 Figure 1 a camshaft adjuster with separate electrical adjusting motor and adjusting gear mechanism, which are connected by a two-side shaft coupling so that they can be disengaged from each other;

- Figure 2 a two-side shaft coupling according to detail X from Figure 1 in cross section;
- 5 Figure 3 a longitudinal section through the two-side shaft coupling from Figure 2;
- Figure 4 a longitudinal section through a two-side shaft coupling similar to Figure 3, but with torque-transferring and rotational back-lash-reducing metal springs;
- 10 Figure 5 a cross section through the two-side shaft coupling from Figure 4;
- 15 Figure 6 a cross section through a two-side shaft coupling similar to Figure 5, but with one-piece spring clasps;
- Figure 7 a longitudinal section through a two-side shaft coupling similar to Figure 4, but with a flat band as a polymer spring;
- 20 Figure 8 a longitudinal section through a two-side shaft coupling similar to Figure 7, but with an O-ring as a polymer spring;
- Figure 9 a cross section X-X through the two-side shaft coupling from Figures 7 and 8;
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- Figure 10 a cross section through a tubular shaft coupling with two opposing, spring-loaded locking balls in separate radial bore holes of a coaxial, cylindrical inner part;
- 5 Figure 11 a cross section through a tubular shaft coupling similar to Figure 10, but with a radial through hole, in which a passage spring is arranged for the two locking balls;
- 10 Figure 12 a cross section through a tubular shaft coupling similar to Figure 10, but with two cylindrical locking pins instead of the two locking balls;
- 15 Figure 13 a cross section through a tubular shaft coupling similar to Figure 11, but with two cylindrical locking pins instead of the two locking balls;
- 20 Figure 14 a longitudinal section through a tubular shaft coupling with a cylindrical inner part, which has on its outer periphery an annular groove, in which an elastically deformable metal tolerance ring is located;
- Figure 15 a partial longitudinal section through a clutch coupling;
- Figure 16 an axial view of the clutch coupling from Figure 15;
- 25 Figure 17 a view of an elastomer collar of the clutch coupling from Figures 15 and 16;

- Figure 18 an axial view of an outer part of a toothed shaft coupling with plastic internal gearing;
- 5 Figure 19 a partial longitudinal section of the outer part from Figure 18 with plastic internal gearing;
- Figure 20 an axial view of an inner part with metal external gearing fitted to the outer part of Figures 18 and 19;
- 10 Figure 21 a side view of the inner part from Figure 20;
- Figure 22 a longitudinal section through a camshaft adjuster similar to Figure 1, but with a magnetic shaft coupling instead of the two-
- 15 side shaft coupling.

DETAILED DESCRIPTION OF THE INVENTION

In Figure 1, an electrical camshaft adjuster 1 is shown, with an adjusting gear mechanism 2 and an electrical adjusting motor 3 which are formed as separate units and can be connected by a coupling so that they can be disengaged from each other.

The adjusting gear mechanism 2 is a three-shaft gear mechanism, which exhibits a high transmission (transmission range from 1:30 to 1:250) and a high efficiency as an eccentric gear mechanism. The adjusting gear mechanism 2 has a drive shaft and a driven shaft, as well as an adjusting shaft 9.

The drive shaft is formed as a chain wheel 5 and is rotationally fixed to a not shown crankshaft by means of a similarly not shown chain. The driven shaft is configured as a closing wall 6, which is rotationally fixed to a camshaft 8 by means of a tension screw 7. The adjusting shaft 9 is formed as an eccentric shaft, which is connected to an adjusting motor shaft 10 in a practically rotational backlash-free manner, but so that it can move in the axial direction, via a two-side shaft coupling 4. The adjusting shaft 9 is used for driving two spur pinions 11, 12, which mesh with internal gearing 13 of the chain wheel 5 and transfer the adjusting moment via pins 14 and via the closing wall 6 to the camshaft 8. The electrical adjusting motor 3 has a stator 15, which is fixed to the cylinder head 16, and a permanent magnet rotor 17, which turns with the camshaft 8.

In Figures 2 and 3, the two-side shaft coupling 4 designated as detail X from Figure 1 is shown enlarged in a cross section and a longitudinal section view. An inner part 18 of the two-side shaft coupling 4 is formed integrally with the adjusting motor shaft 10, and an outer part 19 is formed integrally with the adjusting shaft 9. Both parts 18, 19 each have identical coupling surfaces 20, 21, between which the minimal play required for axial displacement (heat expansion, assembly) is provided. In this way, a minimal rotational backlash is also achieved, which is important for the durability and low-noise operation of the two-side shaft coupling 4, on which changing moments are applied. However, the manufacturing expense required for the minimal backlash and tolerances on both parts 18, 19 is considerable.

This disadvantage is countered by a two-side shaft coupling 4' shown in a longitudinal section and cross section in Figures 4 and 5. Here, a groove 22,

in which a flat bending or a plate spring 23 is inserted with biasing, is provided in the coupling surfaces 20' of each of the inner parts 18'. The springs 23 bridge the now permitted, relatively large play between the inner and outer parts 18', 19' through the biasing and the spring path and take over the transfer of the torque of the adjusting motor 3. Because this torque, at < 1 Nm, is relatively small, the necessary spring and assembly forces are also small and there is no rotation between the adjusting shaft and adjusting motor shaft 9, 10 for the corresponding spring stiffness. Because the torque of the adjusting motor 3 is now transferred via the springs 23, the coupling surfaces 20', 21' do not contact the parts 18', 19'. The springs 23, in connection with the relatively large play between the coupling surfaces 20', 21', are in the position to compensate for small axis offsets between the adjusting shaft and the adjusting motor shaft 9, 10.

Figure 6 shows a coupling 4' as a variant to Figures 4 and 5, for which the two springs 23 and the grooves 22 of the inner part 18' are joined by a spring clip part 24 into a one-piece spring clasp 25, which locks onto corners 26 of the inner part 18' in a way such that it cannot be lost. This loss safety means a considerable simplification in terms of assembly.

In Figures 7 and 8, a two-side shaft coupling 4'' is shown in a longitudinal section and in Figure 9 in a cross section, for which, instead of the flat bending springs or plate springs 23, a polymer band 26 or a polymer O-ring 29 are provided. These are mounted in a circular groove 30, 31 of the inner parts 18' to their coupling surfaces 20' so that they project beyond the surfaces, so that in the installed state, they have biasing. Therefore, the play, which is also large for this variant, between the coupling surfaces 20', 21', is

bridged between the inner and outer parts 18', 19', without these parts coming in contact. Here, the relatively low torque of the adjusting motor 3 is also transferred without relative rotation of the inner and outer parts 18', 19' based on the corresponding stiffness of the polymer band 28 and the polymer O-ring 29.

In Figure 9, the circular groove 30, 31 can be recognized in the inner part 18' with the polymer band 28 and the polymer O-ring 29, which produce an optimum bridging of play between the inner parts 18' and the outer parts 19' of the coupling 4".

Figures 10 to 13 show cross sections through a tubular shaft coupling 32 with a hollow cylindrical outer part 33 and a coaxial, cylindrical inner part 34, which is arranged with play in the hollow cylindrical outer part 33.

In the cylindrical inner part 34 of Figure 10, there are two identical, aligned radial bore holes 35, which extend from its periphery and in which a compression spring 36 is arranged. These springs each act on a locking ball 37, which are guided in the radial bore holes 35 with clearance and displace these balls into another radial bore hole 38 in the outer part 33. The other radial bore holes 38 are aligned in a certain rotational position of the cylindrical inner part 34 with the radial bore holes 35. Due to a certain, minimal diameter of the other radial bore holes 38 in relation to the radial bore holes 35, the locking balls 37 penetrate only up to a certain depth into the other radial bore hole 38, which is sufficient for transferring the torque of the adjusting motor 3. Here, the locking balls are supported on an outer edge 43 of the other radial bore hole 38. Through selection of the diameter

of the other radial bore hole 38, the magnitude of the transferable torque can be defined. In this way, the tubular shaft coupling 32 becomes a safety coupling.

- 5 In Figure 11, the two radial bore holes 35 are replaced by a through hole 39 with a through spring 40. This solution, in comparison with that from Figure 10, has the advantage of minimal construction expense and uniform pressure loading of the two locking balls 37, which permits a more precise fixing of the transferable torque.

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The structure of the tubular shaft couplings 32 of Figures 12 and 13 corresponds to that of Figures 10 and 11. The difference is in the use of cylindrical locking pins 41 instead of locking balls 37, with conical ends 42, which project by means of the pressure force of the compression springs 36' or the through spring 40', in the through hole 39 into other radial bore holes 15 38' and are supported on their outer edges 43'. In this variant, the transferable torque can be limited by the size of the cone angle of the conical ends 42. Therefore, this tubular shaft coupling 32 can also be used as a safety coupling.

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In Figure 14, a tubular shaft coupling 32' is shown as another coupling variant. Here, a non-positive moment transfer between a cylindrical inner part 34' and a hollow cylindrical outer part 33' is achieved through a metallic tolerance ring 44, which is arranged in a radial groove 45 and which is 25 elastically deformable. The tolerance ring 44 projects past the radial groove 45 by a certain extent, which defines the elastic deformation and the dependent force-fit connection.

In Figure 15, a partial cross section through a clutch coupling 46 with claws 47, 48 is shown. These are rotationally fixed on the free ends of the adjusting shaft and adjusting motor shaft 9, 10 at the same diameter. They engage in each other with distances, which are bridged in a rotational backlash-free way by an elastic, biased polymer collar 49 with tooth elements 50 shown in Figure 17.

Figure 16 shows an axial view of the clutch coupling 46, in which eight claws 47 and 48, as well as the polymer collar 49 with eight tooth segments 50, are shown with dashed lines. The clutch coupling 46 compensates for small alignment errors between the adjusting shaft and the adjusting motor shaft 9, 10, and also permits a small axial displacement between the same.

In Figure 18, an axial view of an outer part 55 of a toothed shaft coupling with internal gearing 56 made from elastic plastic is shown. Figure 19 shows a partial longitudinal section of the outer part 55 of Figure 18. The internal gearing 56 is molded into a radial groove 57 of an intermediate bushing 58. In the radial projection, behind each tooth 59 there is a radial bore hole 60, which is filled with plastic and is sealed by a rivet head-like cover 61. The plastic located in the radial bore hole 60 increases the transferable torque of the internal gearing 56. The intermediate bushing 58 can be used as part of the adjusting shaft 9 or the adjusting motor shaft 10 or can be pressed into these parts.

Figures 20 and 21 show a metal inner part 62 with external gearing 63, which have external teeth 64. These are narrower than the plastic internal

teeth 59, because they have a higher strength. Correspondingly, the internal teeth gaps 65 are narrower than the external teeth gaps 66. In principle, the external gearing 63 could also be formed in plastic. However, internal gearing 56 is also possible due to the possibly greater material volume.

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Figure 22 shows a camshaft adjuster 1', whose adjusting shaft 9 is connected in a contact-less and rotational backlash-free way to the adjusting motor shaft 10' by a permanent magnet shaft coupling 51. Permanent magnets 52, 53 are fixed to the free ends of the adjusting shaft and the adjusting motor shaft 9, 10'. Between these magnets, there is a non-magnetic membrane 54, which closes the adjusting motor 3 in an oil-tight way. In this way, the adjusting motor 3 is hermetically sealed without friction-generating sealing elements.

List of reference symbols

	1, 1'	Camshaft adjuster
	2	Adjusting gear mechanism
5	3	Electrical adjusting motor
	4, 4', 4''	Two-side shaft coupling
	5	Chain wheel
	6	Closing wall
	7	Tension screw
10	8	Camshaft
	9	Adjusting shaft
	10, 10'	Adjusting motor shaft
	11	Spur pinion
	12	Spur pinion
15	13	Internal gearing
	14	Pin
	15	Stator
	16	Cylinder head
	17	Permanent magnet rotor
20	18, 18'	Inner part
	19, 19'	Outer part
	20, 20'	Coupling surface
	21, 21'	Coupling surface
	22	Groove
25	23	Flat bending or plate spring
	24	Spring clip
	25	Spring clasp

	26	Corner
	27	Transverse groove
	28	Polymer band
	29	Polymer O-ring
5	30	Circular groove
	31	Circular groove
	32, 32'	Tubular shaft coupling
	33, 33'	Hollow cylindrical outer part
	34, 34'	Coaxial, cylindrical inner part
10	35	Radial bore hole
	36, 36'	Compression spring
	37	Locking ball
	38, 38'	Other radial bore hole
	39	Through hole
15	40, 40'	Through spring
	41	Cylindrical locking pin
	42	Conical end
	43, 43'	Outlet edge
	44	Tolerance ring
20	45	Radial groove
	46	Clutch coupling
	47	Claw
	48	Claw
	49	Polymer collar
25	50	Tooth element
	51	Permanent magnet shaft coupling
	52	Permanent magnet

	53	Permanent magnet
	54	Membrane
	55	Outer part
	56	Internal gearing
5	57	Radial groove
	58	Intermediate bushing
	59	Internal tooth
	60	Radial bore hole
	61	Cover
10	62	Inner part
	63	External gearing
	64	External tooth
	65	Internal teeth gaps
	66	External teeth gaps